Parameterized Quasi-Physical Simulators for Dexterous Manipulations Transfer

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Fig. 1: By optimizing through a **quasi-physical simulator curriculum**, we successfully transfer human demonstrations to dexterous robot hand simulations. We enable accurate tracking of complex manipulations with changing contacts (*Fig. (a)*), non-trivial object motions (*Fig. (b)*) and intricate tool-using (*Fig. (c,d)*). Besides, our physics curriculum can substantially improve the performance of a failed baseline as well (*Fig. (e,f)*).

Abstract. We explore the dexterous manipulation transfer problem by designing simulators. The task wishes to transfer human manipulations to dexterous robot hand simulations and is inherently difficult due to its intricate, highly-constrained, and discontinuous dynamics and the need to control a dexterous hand with a DoF to accurately replicate hu-man manipulations. Previous approaches that optimize in high-fidelity black-box simulators or a modified one with relaxed constraints only demonstrate limited capabilities or are restricted by insufficient simula-tion fidelity. We introduce parameterized quasi-physical simulators and a **physics curriculum** to overcome these limitations. The key ideas are 1) balancing between fidelity and optimizability of the simulation via a curriculum of parameterized simulators, and 2) solving the problem in each of the simulators from the curriculum, with properties ranging from high task optimizability to high fidelity. We successfully enable a dex-terous hand to track complex and diverse manipulations in high-fidelity simulated environments, boosting the success rate by 11%+ from the best-performed baseline. We include a website to introduce the work.

022 Keywords: Dexterous Manipulation Transfer · Hybrid Simulation

023 1 Introduction

Advancing an embodied agent's capacity to interact with the world represents a significant stride toward achieving general artificial intelligence. Due to the substantial costs and potential hazards of setting up real robots to do trial and error, the standard approach for developing embodied algorithms involves learning in physical simulators [9, 15, 23, 25, 33, 56, 59] before transitioning to real-world deployment. In most cases, physical simulators are treated as black boxes, and extensive efforts have been devoted to developing learning and op-timization methods for embodied skills within these black boxes. Despite the considerable progress [2, 6–8, 16, 20, 21, 31, 36, 39, 43, 46, 60, 62, 66, 68], the question like whether the simulators used are the most suitable ones is rarely discussed. In this work, we investigate this issue and illustrate how optimizing the simulator concurrently with skill acquisition can benefit a popular vet challenging task in robot manipulation – dexterous manipulation transfer.

The task aims at transferring human-object manipulations to a dexterous robot hand, enabling it to physically track the reference motion of both the hand and the object (see Fig. 1). It is challenged by 1) the complex, highly con-strained, non-smooth, and discontinuous dynamics with frequent contact estab-lishment and breaking involved in the robot manipulation. 2) the requirement of precisely controlling a dexterous hand with a high DoF to densely track the ma-nipulation at each frame, and 3) the morphology difference. Some existing works rely on high-fidelity black-box simulators, where a small difference in robot con-trol can result in dramatically different manipulation outcomes due to abrupt contact changes, making the tracking objective highly non-smooth and hard to optimize [4, 6, 8, 43, 46]. In this way, their tasks are restricted to relatively simple goal-driven manipulations such as pouring and re-locating [8, 43, 46, 68], in-hand re-orientation, flipping and spinning [4, 6] with a fixed-root robot hand, or ma-nipulating objects with simple geometry such as balls [36]. Other approaches attempt to improve optimization by relaxing physical constraints, with a pri-mary focus on smoothing out contact responses [3, 24, 38, 55, 56]. However, their dynamics models may significantly deviate from real physics [38], hindering skill deployment. Consequently, we ask how to address the optimization challenge while preserving the high fidelity of the simulator.

Our key insight is that a single simulator can hardly provide both high fidelity and excellent optimizability for contact-rich dexterous manipulations. Inspired by the line of homotopy methods [12, 28, 29, 61], we propose a curriculum of simulators to realize this. We start by utilizing a quasi-physical simulator to initially relax physical constraints and warm up the optimization. Subsequently, we transfer the optimization outcomes to simulators with gradually tightened physical constraints. Finally, we transition to a physically realistic simulator for skill deployment in realistic dynamics.

064To realize this vision, we propose a family of parameterized quasi-
physical simulators for contact-rich dexterous manipulation tasks. These sim-
ulators can be customized to enhance task optimizability while can also be tai-
lored to approximate realistic physics. The parameterized simulator represents064
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an articulated multi rigid body as a parameterized point set, models contact using an unconstrained parameterized spring-damper, and compensates for un-modeled effects via parameterized residual physics. Specifically, the articulated multi-body dynamics model is relaxed as the point set dynamics model. An ar-ticulated object is relaxed into a set of points, sampled from the ambient space surrounding each body's surface mesh. The resulting dynamics model combines the original articulated dynamics with the mass-point dynamics of each indi-vidual point. Parameters are introduced to control the point set construction and the dynamics model. The contact model is softened as a parameterized spring-damper model [3, 19, 35, 38, 51] with parameters introduced to control when to calculate contacts and contact spring stiffness. The residual physics network compensate for unmodeled effects from the analytical modeling [22]. The parameterized simulator can be programmed for high optimizability by re-laxing constraints in the analytical model and can be tailored to approximate realistic physics by learning excellent residual physics. We demonstrate that the challenging dexterous manipulation transfer task can be effectively addressed through curriculum optimization using a series of parameterized physical simu-lators. Initially, both articulated rigid constraints and the contact model stiffness are relaxed in the simulator. It may not reflect physical realism but provides a good environment where the manipulation transfer problem can be solved eas-ily. Subsequently, the articulated rigid constraints and the contact model are gradually tightened. Task-solving proceeds iteratively within each simulator in the curriculum. Finally, the parameterized simulator is optimized to approxi-mate realistic physics. Task optimization continues, yielding a dexterous hand trajectory capable of executing the manipulation in environments with realistic physics.

We demonstrate the superiority of our method and compare it with previ-ous model-free and model-based methods on challenging manipulation sequences from three datasets, describing single-hand or bimanual manipulations with daily objects or using tools. We conduct dexterous manipulation transfer on two widely used simulators, namely Bullet [9] and Isaac Gym [33] to demon-strate the generality and the efficacy of our method and the capability of our quasi-physical simulator to approximate the unknown black-box physics model in the contact-rich manipulation scenario (Fig. 1). We can track complex manip-ulations involving non-trivial object motions such as large rotations and com-plicated tool-using such as using a spoon to bring the water back and forth. Our approach successfully surpasses the previous best-performed method both quantitatively and qualitatively, achieving more than 11% success rate than the previous best-performed method. Besides, optimizing through the physics cur-riculum can significantly enhance the performance of previously under-performed RL-based methods, almost completing the tracking problem from failure, as demonstrated in Fig. 1. This indicates the universality of our approach to em-bodied AI through optimization via a physics curriculum. Thorough ablations are conducted to validate the efficacy of our designs.

- 113- We introduce a family of parameterized quasi-physical simulators that can113114be configured to relax various physical constraints, facilitating skill optimiza-114115tion, and can also be tailored to achieve high simulation fidelity.115
- 116- We present a quasi-physics curriculum along with a corresponding opti-
mization method to address the challenging dexterous manipulation transfer116117problem.118
- Extensive experiments demonstrate the effectiveness of our method in trans ferring complex manipulations, including non-trivial object motions and
 changing contacts, to a dexterous robot hand in simulation.

122 2 Related Works

Dexterous manipulation transfer. Transferring human manipulations to dexterous robot-hand simulations is an important topic in robot skill acquisi-tion [8,21,31,43,60,62,68,70]. Most approaches treat the simulator as black-box physics models and try to learn skills directly from that [4, 6, 8, 43, 46]. However, their demonstrated capabilities are restricted to relatively simple tasks. Another trend of work tries to relax the physics model [37, 38] to create a better environ-ment for task optimization. However, due to the disparity between their mod-eling approach and realistic physics, successful trials are typically demonstrated only in their simulators, which can hardly complete the task under physically realistic dynamics. In this work, we introduce various parameterized analytical relaxations to improve the task optimizability while compensating for unmodeled effects via residual physics networks so the fidelity would not be sacrificed.

Learning for simulation. Analytical methods can hardly approximate an ex-tremely realistic physical world despite lots of smart and tremendous efforts made in developing numerical algorithms [19, 23, 26, 27]. Recently, data-driven approaches have attracted lots of interest for their high efficiency and strong approximation ability [10, 11, 22, 40, 41, 50, 63]. Special network designs are pro-posed to learn the contact behaviour [22,41]. We in this work propose to leverage an analytical-neural hybrid approach and carefully design network modules for approximating residual contact forces in the contact-rich manipulation scenario. Sim-to-Sim and Sim-to-Real transfer. The field of robot manipulation con-tinues to face challenges in the areas of Sim2Sim and Sim2Real transferabil-ity [71]. Considering the modeling gaps, the optimal strategy learned in a specific simulator is difficult to transfer to a different simulator or the real world. There-fore, many techniques for solving the problem have been proposed, including imitation learning [34, 42, 43, 45, 46, 48], transfer learning [72], distillation [47, 57], residual physics [17, 67], and efforts on bridging the gap from the dynamics model aspect [22, 69]. Our parameterized simulators learn residual physics involved in contact-rich robot manipulations. By combining an analytical base with residual networks, we showcase their ability to approximate realistic physics.

153 3 Method

Given a human manipulation demonstration, composed of a human hand mesh trajectory and an object pose trajectory $\{\mathcal{H}, \mathcal{O}\}$, the goal is transferring the 155



Fig. 2: The parameterized quasi-physical simulator relaxes the articulated multi rigid body dynamics as the *parameterized point set dynamics*, controls the contact behavior via an unconstrained *parameterized spring-damper contact model*, and compensates for unmodeled effects via *parameterized residual physics networks*. We tackle the difficult dexterous manipulation transfer problem via **a physics curriculum**.

demonstration to a dexterous robot hand in simulation. Formally, we aim to optimize a control trajectory \mathcal{A} that drives the dexterous hand to manipulate the object in a realistic simulated environment so that the resulting hand trajectory $\hat{\mathcal{H}}$ and the object trajectory $\hat{\mathcal{O}}$ are close to the reference motion $\{\mathcal{H}, \mathcal{O}\}$. The problem is challenged by difficulties from the highly constrained, discontinuous, and non-smooth dynamics, the requirement of controlling a high DoF dexterous hand for tracking, and the morphology difference.

Our method comprises two key designs to tackle the challenges: 1) a family of parameterized quasi-physical simulators, which can be programmed to enhance the optimizability of contact-rich dexterous manipulation tasks and can also be tailored to approximate realistic physics (Section 3.1), and 2) a physics curricu-lum that carefully adjusts the parameters of a line of quasi-physical simulators and a strategy that solves the difficult dexterous manipulation transfer task by addressing it within each simulator in the curriculum (Section 3.2).

170 3.1 Parameterized Quasi-Physical Simulators

Our quasi-physical simulator represents an articulated multi-body, *i.e.*, the robotic dexterous hand, as a point set. The object is represented as a signed distance field. The base of the simulator is in an analytical form leveraging an uncon-strained spring-damper contact model. Parameters are introduced to control the analytical relaxations on the articulated rigid constraints and the softness of the contact model. Additionally, neural networks are introduced to compensate for unmodeled effects beyond the analytical framework. We will elaborate on each of these design aspects below.

Parameterized point set dynamics. Articulated multi-body represented in the reduced coordinate system [19,59] may require a large change in joint states to achieve a small adjustment in the Euclidean space. Moving the end effector from one point to a nearby point may require adjusting all joint states (Fig. 3). Besides, transferring the hand trajectory to a morphologically different hand requires correspondences to make the resulting trajectory close to the original one. Defining correspondences in the reduced coordinate or via sparse correspon-

dences will make the result suffer from noise in the data, leading to unwanted results finally (Fig. 3). Hence, we propose relaxing an articulated multi-rigid body into a mass-point set sampled from the ambient space surrounding each body. Each point is considered attached to the body from which it is sampled and is capable of both self-actuation and actuation via joint motors. We intro-duce a parameter α to control the point set construction and the dynamics. This representation allows an articulated rigid object to behave similarly to a deformable object, providing a larger action space to adjust its state and thereby easing the control optimization problem.

Specifically, for each body of the articulated ob-ject, we sample a set of points from the ambient space near the body mesh. The point set \mathcal{Q} is con-structed by concatenating all sampled points to-gether. Each point $\mathbf{p}_i \in \mathcal{Q}$ is treated as a mass point with a finite mass \mathbf{m}_i and infinitesimal vol-ume. The dynamics of the point set consist of artic-ulated multi-body dynamics [14, 30], as well as the mass point dynamics of each point \mathbf{p}_i . For each \mathbf{p}_i , we have:



where \mathbf{J}_i represents the Jacobian mapping from the generalized velocity to the point velocity $\dot{\mathbf{x}}_i$, \mathbf{u} denotes the generalized joint force, \mathbf{f}_i accounts for ex-

ternal forces acting on \mathbf{p}_i , and $\mathbf{a}_i \in \mathbb{R}^3$ represents the actuation force applied to the point \mathbf{p}_i . Consequently, the point set is controlled by a shared control in the reduced coordinate space \mathbf{u} and per-point actuation force \mathbf{a}_i .

Parameterized spring-damper contact modeling. To ease the optimization challenges posed by contact-rich manipulations, which arise from contact con-straints such as the non-penetration requirement and Coulomb friction law [3, 5]. as well as discontinuous dynamics involving frequent contact establishment and breaking, we propose a parameterized contact model for relaxing constraints and controlling the contact behavior. Specifically, we leverage a classical un-constrained spring-damper model [19, 35, 51, 59, 64] to model the contacts. This model allows us to flexibly adjust the contact behavior by tuning the contact threshold and the spring stiffness coefficients. Intuitively, a contact model with a high threshold and low spring stiffness presents "soft" behaviors, resulting in a continuous and smooth optimization space. This makes optimization through such a contact model relatively easy. Conversely, a model with a low threshold and large stiffness coefficients will produce "stiff" behaviors, increasing the dis-continuity of the optimization space due to frequent contact establishment and breaking. However, it also becomes more physically realistic, meaning contact forces are calculated only when two objects collide, and a large force is applied to separate them if penetrations are observed, thus better satisfying the non-penetration condition. Therefore, by adjusting the contact distance threshold



Fig. 3: Point Set can flexibly adjust its states, avoid overfitting to data noise, and ease the difficulty brought by the morphology difference. and spring stiffness coefficients, we can modulate the optimizability and fidelity of the contact model. The parameter set of the contact model comprises a distance threshold d^c and spring stiffness coefficients. Next, we will delve into the details of the contact establishment, breaking, and force calculations processes.

Contacts are established between points in the manipulator's point set \mathcal{O} 234 234 and the object. A point $\mathbf{p} \in \mathcal{O}$ is considered to be in "contact" with the object 235 235 if its signed distance to the object $sd(\mathbf{p})$ is smaller than the contact distance 236 236 threshold d^c . Subsequently, the object surface point nearest to **p** is identified as 237 237 the corresponding contact point on the object, denoted as \mathbf{p}^{o} . The normal direc-238 238 tion of the object point \mathbf{p}^{o} is then determined as the contact normal direction, 239 239 denoted as \mathbf{n}^{o} . The contact force \mathbf{f}^{c} applied from the manipulator point \mathbf{p} to \mathbf{p}^{o} 240 240 is calculated as follows: 241 241

$$\mathbf{f}^c = -(k^n d - k^d d\dot{d})\mathbf{n}^o,\tag{2}$$

where, k^n represents the spring stiffness coefficient, k^d denotes the damping coefficient, and $d = d^c - \operatorname{sd}(\mathbf{p})$ is always positive. To enhance the continuity of \mathbf{f}^c [64], $k^d d\dot{d}$ is used as the magnitude of the damping force, rather than $k^d \dot{d}$.

Friction forces are modeled as penalty-based spring forces [3,65]. Once a point p is identified as in contact with the object, with the object contact point denoted as \mathbf{p}^{o} , the contact pair is stored. Contact forces between them are continually calculated until the contact breaking conditions are met. In more detail, the static friction force from \mathbf{p} to \mathbf{p}^{o} is calculated using a spring model: 250

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$$\mathbf{f}_s^f = k^f \mathbf{T}_n (\mathbf{p} - \mathbf{p}^o), \qquad (3) \quad 251$$

where k^f is the friction spring stiffness coefficient, $\mathbf{T}_n = \mathbf{I} - \mathbf{n}^o \mathbf{n}^{oT}$ is a tangential projection operator. When the static friction satisfies $\|\mathbf{f}_s^f\| \le \mu \|\mathbf{f}^c\|$, \mathbf{f}_s^f is applied to the object point \mathbf{p}^o . Otherwise, the dynamic friction force is applied, and the contact breaks:

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$$\mathbf{f}_{d}^{f} = -\mu \|\mathbf{f}_{s}^{f}\| \frac{\mathbf{T}_{n} \mathbf{v}_{\mathbf{p} \leftarrow \mathbf{p}^{o}}}{\|\mathbf{T}_{n} \mathbf{v}_{\mathbf{p} \leftarrow \mathbf{p}^{o}}\|},\tag{4}$$

257 where $\mathbf{v}_{\mathbf{p}\leftarrow\mathbf{p}^o}$ is the relative velocity between \mathbf{p} and \mathbf{p}^o .

Parameterized residual physics. The analytical designs facilitate relaxation
but may limit the use of highly sophisticated and realistic dynamics models,
deviating from real physics. To address this, the final component of our quasiphysical simulator is a flexible neural residual physics model [1, 22, 41].

Specifically, we propose to use networks to learn to predict residual con-262 262 tact forces and friction forces from contact-related information. For fine-grained 263 263 residual contact force prediction, we design a local contact network $f_{\eta_{n-1}}$ that 264 264 inherits contact information identified in the parameterized contact model and 265 265 predicts residual forces between each contact pair. To close the gap caused by 266 266 contact region identification between the parameterized contact model and real 267 267 contact region, we further include a global residual network $f_{\psi_{\text{global}}}$ that predicts 268 268 residual forces and torques added directly to the object's center of mass. In more 269 269 detail, given a contact pair $(\mathbf{p}, \mathbf{p}^o)$, the local contact network maps the contact-270 270 related features of the local contact region, consisting of geometry, per-point 271 271 velocity, and per object point normal, to the residual contact force and residual 272 272

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friction force between such two points in the contact pair. The global residual network additionally takes contact-related information of the global contact re-gion, including the geometry, per-point velocity, and per-object point normal. as input and predicts a residual force and residual torque added to the object's center of mass. Details such as contact region identification and network ar-chitectures are deferred to the Supp. We denote the optimizable parameters in the residual physics network as $\psi = (\psi_{global}, \psi_{local})$. By optimizing the resid-ual physics network, we unlock the possibility of introducing highly non-linear dynamics to align our parametrized quasi-physical simulator with any realistic black-box physical simulator.

283 Semi-implicit time-stepping is leveraged to make the simulation auto differ-284 entiable and easy to combine with neural networks [22]. 284

3.2 Dexterous Manipulation Transfer via a Physics Curriculum

Based on the family of parameterized quasi-physical simulators, we propose to solve the challenging dexterous manipulation transfer problem via a physics cur-riculum. It is constructed by a series of parameterized simulators varying from the one with few constraints and the softest contact behavior, gradually to a re-alistic simulator. We then solve the problem by transferring the demonstration to the dexterous hand in each simulator across the curriculum gradually. In more detail, the optimization starts from the parameterized simulator with both the articulated rigid constraints removed and the contact model tuned to the softest level. The residual physics networks are deactivated. It provides a friendly envi-ronment for optimization, and we can easily arrive at a workable hand trajectory here. Then the physics is gradually tightened and we solve the task in each sim-ulator. After reaching the most tightened analytical model, the analytical part is fixed and residual networks are activated. The simulator is gradually opti-mized to approximate the dynamics in a realistic physical environment. At the same time, the control trajectory \mathcal{A} continues to be refined in the quasi-physical simulator. Finally, we arrive at a simulator optimized to be with high fidelity and a trajectory \mathcal{A} that can drive the dexterous hand to physically track the demonstration in a realistic simulated physical environment. Additionally, since object properties as well as system parameters like linear and angular velocity damping coefficients are unknown from the kinematics-only demonstration, we set them optimizable and identify them (denoted \mathcal{S}) together with optimizing the hand control trajectory. Next we'll illustrate this in detail.

Transferring human demonstration via point set dynamics. To robustly transfer the human demonstration to a morphologically different dexterous robot hand in simulation and to overcome noise in the kinematic trajectory, we ini-tially relax the articulated rigid constraints and transfer the kinematics human demonstration to the control trajectory of the point set. Specifically, the point set representation with the relaxation parameter α for the dynamic human hand [8] is constructed. The shared control trajectory \mathcal{A} and per-point per-frame actions are optimized so that the resulting trajectory of the point set can manipulate the object according to the demonstration. After that, a point set with the same

parameter α is constructed to represent the dexterous robot hand. Subsequently, the shared control trajectory \mathcal{A} and per-point per-frame actions are optimized

319 to track the manipulation accordingly.

Transferring through a contact model curriculum. After that, the articu-lated rigid constraint is tightened by freezing the point set parameter α to zero. The following optimization starts from a parameterized simulator with the soft-est contact model. We then gradually tighten the contact model by adjusting its distance threshold, contact force spring stiffness, etc. By curriculum optimizing the trajectory \mathcal{A} and parameters \mathcal{S} in each of the quasi-physical simulators, we finally arrive at the control trajectory that can drive a dexterous hand to accom-plish the tracking task in the parameterized simulator with the most tightened analytical model.

Optimizing towards a realistic physical environment. Subsequently, the residual physics network is activated and the parameterized simulator is opti-mized to approximate the dynamics in a realistic physical environment. We con-tinue to optimize the hand trajectory in the quasi-physical simulator. Specifically, we leverage the successful trial in model-based human tracking literature [16,66] and iteratively optimize the control trajectory \mathcal{A} and the parameterized simu-lator. In more detail, the following two subproblems are iteratively solved: 1) optimizing the quasi-physical simulator to approximate the realistic dynamics. and 2) optimizing the control trajectory \mathcal{A} to complete the manipulation in the quasi-physical simulator. Gradient-based optimization is leveraged taking advantage of the differentiability of the parameterized simulator.

After completing the optimization, the final control trajectory is yielded by model predictive control (MPC) [18] based on the optimized parameterized simulator and the hand trajectory \mathcal{A} . Specifically, in each step, the current and the following controls in several subsequent frames are optimized to reduce the tracking error. More details are deferred to the Supp.

345 4 Experiments

We conduct extensive experiments to demonstrate the effectiveness of our method. The evaluation dataset is constructed from three HOI datasets with both single-hand and bimanual manipulations (with rigid objects), with complex manipula-tions with non-trivial object movements, and rich and changing contacts involved (see Section 4.1). We use Shadow hand [49] and test in two simulators widely used in the embodied AI community: Bullet [9] and Isaac Gym [33]. We com-pare our method with both model-free approaches and model-based strategies and demonstrate the superiority of our method both quantitatively and qual-itatively. We can track complex contact-rich manipulations with large object rotations, back-and-forth object movements, and changing contacts successfully in both of the two simulators, while the best-performed baseline fails (see Sec-tion 4.2, Fig. 4). On average, we boost the tracking success rate by 11%+ from the previous best-performed (see Section 4.2). We make further analysis and dis-cussions and show that the core philosophy of our work, optimizing through a quasi-physics curriculum, is potentially general and can help improve the per-formance of a model-free baseline (see Section 4.3).



Fig. 4: Qualitative comparisons. Please refer to our website and the supplementary video for animated results.

362 4.1 Experimental Settings

Datasets. Our evaluation dataset is compiled from three distinct sources, namely 363 363 GRAB [53], containing single-hand interactions with daily objects, TACO [32], 364 364 containing humans manipulating tools, and ARCTIC [13] with bimanual manip-365 365 ulations. For GRAB, we randomly sample a manipulation trajectory for each 366 366 object. If its manipulation is extremely simple, we additionally sample one tra-367 367 jectory for it. The object is not considered if its corresponding manipulation 368 368 is bimanual such as **binoculars**, involves other body parts such as **bowl**, or 369 369 with detailed part movements such as the game controller. The number of 370 370 manipulation sequences from GRAB is 27. For TACO [32], we acquire data by 371 371 contacting authors. We randomly select one sequence for each right-hand tool ob-372 372 ject. Sequences with very low quality like erroneous object motions are excluded. 373 373 14 trajectories in total are selected finally. For ARCTIC [13], we randomly se-374 374 lect one sequence for each object from its available manipulation trajectories, 375 375 resulting in 10 sequences in total. More details are deferred to the Supp. 376 376

Metrics. We introduce three distinct metrics to assess the quality of object 377 tracking, the accuracy of hand tracking, and the overall success of the tracking 378 task: 1) Per-frame average object rotation error: $R_{\rm err} = \frac{1}{N} \sum_{n=1}^{N} (1 - (\mathbf{q}_n \cdot \hat{\mathbf{q}}_n)),$ 379

where \mathbf{q}_n is the ground-truth orientation and $\hat{\mathbf{q}}_n$ is the tracked result, rep-resented in quaternion. 2) Per-frame average object translation error: $T_{\rm err} =$ $\frac{1}{N}\sum_{n=1}^{N} \|\mathbf{t}_n - \hat{\mathbf{t}}_n\|$, where \mathbf{t} and \mathbf{t}_n are ground-truth and tracked translations re-spectively. 3) Mean Per-Joint Position Error (MPJPE) = $\frac{1}{N} \sum_{n=1}^{N} \|\mathbf{J}_n - \hat{\mathbf{J}}_n\|$ [20, 44,58], where \mathbf{J}_n and $\hat{\mathbf{J}}_n$ are keypoints of GT human hand and the simulated robot hand respectively. We manually define the keypoints and the correspon-dences to the human hand keypoints for the Shadow hand. 4) Per-frame aver-age hand Chamfer Distance: $CD = \frac{1}{N} \sum_{n=1}^{N} Chamfer-Distance(\mathbf{H}_n - \hat{\mathbf{H}}_n)$, for evaluating whether the Shadow hand can "densely" track the demonstration. 5) Success rate: a tracking is regarded as successful if the object rotation er-ror $R_{\rm err}$, object translation error $T_{\rm err}$, and the hand tracking error MPJPE are smaller than their corresponding threshold. Three success rates are calculated using three different thresholds, namely $10^{\circ} - 10cm - 10cm$, $15^{\circ} - 15cm - 15cm$. **Baselines.** We compare with two trends of baselines. For model-free approaches, since there is no prior work with exactly the same problem setting as us, we try to modify and improve a goal-driven rigid object manipulation method DGrasp [8] into two methods for tracking: 1) DGrasp-Base, where the method is almost kept with same with the original DGrasp. We use the first frame where the hand and the object are in contact with each other as the reference frame. Then the policy is trained to grasp the object according to the reference hand and object goal at first. After that, only the root is guided to complete the task. 2) DGrasp-Tracking, where we divide the whole sequence into several subsequences, each of which has 10 frames, and define the end frame of the subsequence as the reference frame. Then the grasping policy is used to guide the hand and gradually track the object according to the hand and the object pose of each reference frame. We improve the DGrasp-Tracking by optimizing the policy through the quasi-physical curriculum and creating "DGrasp-Tracking (w/ Curriculum)" trying to improve its performance. For model-based methods, we compare with Control-VAE [66] and traditional MPC approaches. For Control-VAE, we modify its implementation for the manipulation tracking task. We additionally consider three differentiable physics models to conduct model-predictive control for solv-ing the task. Taking the analytical model with the most tightened contact model as the base model ("MPC (w/ base sim.)"), we further augment it with a general state-of-the-art contact smoothing for robot manipulation [52] and create "MPC (w/ base sim. w/ soften)". Details of baseline models are deferred to the Supp. **Training and evaluation settings.** The physics curriculum is composed of

three stages. In the first stage, the parameter α varies from 0.1 to 0.0 and the contact model stiffness is relaxed to the softest level. In the second stage, α is fixed and the contact model stiffness varies from the softest version to the most tightened level gradually through eight stages. Details w.r.t. parameter settings are deferred to the Supp. In the first two stages, we alternately optimize the trajectory \mathcal{A} and parameters \mathcal{S} . In each optimization iteration, the \mathcal{A} is optimized for 100 steps while S is optimized for 1000 steps. In the third stage, A and ψ are optimized for 256 steps in each iteration. For time-stepping, dt is set to 5×10^{-4} in the parameterized and the target simulators. The articulated multi-body is

Simulator		Method	R_{err} (°, \downarrow)	$T_{\rm err} \ (cm,\downarrow)$	MPJPE (mm,\downarrow)	CD $(mm,\downarrow$) Success Rate $(\%,\uparrow)$
Bullet	Model Free	DGrasp-Base	44.24	5.82	40.55	16.37	0/13.73/15.69
		DGrasp-Tracking	44.45	5.04	37.56	14.72	0/15.69/15.69
		DGrasp-Tracking (w/ curric.)	33.86	4.60	30.47	13.53	7.84/23.53/37.25
	Model	Control-VAE	42.45	2.73	25.21	10.94	0/15.68/23.53
	Based	MPC (w/ base sim.)	32.56	3.67	24.62	10.80	0/15.68/31.37
		MPC (w/ base sim. w/ soften)	31.89	3.63	28.26	11.31	0/21.57/37.25
		Ours	24.21	1.97	24.40	9.85	27.45 / 37.25 / 58.82
Isaac Gym	Model Free	DGrasp-Base	36.41	4.56	50.97	18.78	0/7.84 /7.84
		DGrasp-Tracking	44.71	5.57	41.53	16.72	0/0/7.84
		DGrasp-Tracking (w/ curric,)	38.75	5.13	40.09	16.26	0/23.53/31.37
	Model Based	Control-VAE	35.40	4.61	27.63	13.17	0/13.73/29.41
		MPC (w/ base sim.)	37.23	4.73	23.19	9.75	0/15.69/ <i>31.37</i>
		MPC (w/ base sim. w/ soften)	36.40	4.46	23.27	10.34	0/9.80/23.53
		Ours	25.97	2.08	25.33	10.31	21.57/43.14/56.86

Table 1: Quantitative evaluations and comparisons to baselines. Bold red numbers for best values and *italic blue* values for the second best-performed ones.

controlled by joint motors and root velocities in the parameterized quasi-physical
simulator while PD control [54] is leveraged in the target simulators.

427 4.2 Dexterous Manipulating Tracking

We conducted thorough experiments in two widely used simulators [9, 33]. We treat them as realistic simulated physical environments with high fidelity and wish to track the manipulation in them. In summary, we can control a dexterous hand to complete a wide range of the manipulation tracking tasks with non-trivial object movements and changing contacts. As presented in Table 1, we can achieve significantly higher success rates calculated under three thresholds than the best-performed baseline in both tested simulators. Fig. 4 showcases qualitative examples and comparisons. Please refer to our website and supple-mentary video for animated results.

Complex manipulations. For examples shown in Fig. 4, we can complete the tracking task on examples with large object re-orientations and complicated tool-using (Fig. (a,b,c)). However, DGrasp-Tracking fails to establish sufficient contact for correctly manipulating the object. In more detail, in Fig. 4(b), the bunny gradually bounced out from its hand in Bullet, while our method does not suffer from this difficulty. In Fig. 4(c), the spoon can be successfully picked up and waved back-and-forth in our method, while DGrasp-Tracking loses the track right from the start.

Bimanual manipulations. We are also capable of tracking bimanual manipu-445446lations. As shown in the example in Fig. 4(d), where two hands collaborate to446447relocate the object, DGrasp-Tracking fails to accurately track the object, while447448our method significantly outperforms it.448

449 4.3 Further Analysis and Discussions

450 Could model-free methods benefit from the physics curriculum? In ad451 dition to the demonstrated merits of our quasi-physical simulators, we further
452 explore whether model-free strategies can benefit from them. We introduce the
453 "DGrasp-Tracking (w/ Curriculum)" method and compare its performance with
453

Method	$R_{\rm err}$ (°, \downarrow)	$T_{\rm err} (cm,\downarrow)$) MPJPE (mm,\downarrow)	CD (mm,\downarrow)) Success Rate $(\%,\uparrow)$
Ours w/o Analytical Sim.	44.27	4.39	29.84	12.91	0/13.73/25.49
Ours w/o Residual Physics	33.69	3.81	26.57	10.34	5.88/23.53/41.18
Ours w/o Local Force NN	35.98	2.90	32.87	12.44	0/19.61/35.29
Ours w/o Curriculum	42.40	4.87	32.61	13.37	0/17.64/29.41
Ours w/ Curriculum II	29.58	2.33	31.61	10.29	11.76/27.45/50.98
Ours	24.21	1.97	24.40	9.85	27.45/37.25/58.82

Table 2: Ablation studies. Bold red numbers for best values and *italic blue* values for the second best-performed ones. The simulation environment is Bullet.

the original DGrasp-Tracking model. As shown in Table 1 and the visual comparisons in Fig. 6, the DGrasp-Tracking model indeed benefits from a well-designed
physics curriculum. For example, as illustrated in Fig. 6, the curriculum can
significantly improve its performance, enabling it to nearly complete challenging
tracking tasks where the original version struggles.

459 5 Ablation Study



Fig. 5: (a) Qualitative comparisons between our full method and the ablated models; (b) Training loss curve comparisons; (c) Tracking loss curve comparisons.



Fig. 6: Visual evidence on boosting DGrasp-Tracking's performance via optimizing it through a physics curriculum.

We conduct a wide range of ablation studies to validate the effectiveness defined of some of our crucial designs, including the parameterized analytical physics defined model, the parameterized residual physics, the role of the local force network, defined defined

the necessity of introducing a physics curriculum into the optimization, and how
the design on the curriculum stages affects the result.

Parameterized analytical model. The skeleton of the quasi-physical simu-lator is an analytical physics model. The intuition is that the parameterized simulator with such physical bias can be optimized towards a realistic simulator more easily than training pure neural networks for approximating. To validate this, we ablate the analytical model and use neural networks to approximate physics in Bullet directly (denoted as "Ours w/o Analytical Sim."). The quanti-tative (Table 2) and qualitative (Fig. 5) results indicate that the physical biases brought by the analytical model could help the parameterized simulator to learn better physics in the contact-rich scenario. For instance, in the example demon-strated in Fig. 5, the ablated version fails to guide the robot hand to successfully pinch the object in the second figure.

Parameterized residual physics. To validate the necessity of introducing residual force networks to close the gap between the physics modeled in the parameterized analytical simulator and that of a realistic simulator, we ablate the parameterized force network and create a version named "Ours w/o Residual Physics". Table 2 demonstrated its role in enabling the parameterized simulator to approximate realistic physics models.

Local residual force network. To adequately leverage state and contact-related information for predicting residual contact forces, we propose to use two types of networks: 1) a local force network for per contact pair residual forces and 2) a global network for additionally compensating. The local network is introduced for fine-grained approximation. We ablate this design and compare the result with our full model to validate this (see Fig. 5 and Table 1).

Optimizing through an analytical physics curriculum. We further inves-tigate the effectiveness of the analytical curriculum design and how its design influences the result. Specifically, we create two ablated versions: 1) "Ours w/oCurriculum", where the optimization starts directly from the parameterized ana-lytical model with articulated rigid constraints tightened and the stiffest contact model, and 2) "Ours w/ Curriculum II", where we move some stages out from the original curriculum. Table 2 and Fig. 5 demonstrate that both the curriculum and the optimization path will affect the model's performance.

⁴⁹⁶ 6 Conclusion and Limitations

In this work, we investigate creating better simulators for solving complex robotic tasks involving complicated dynamics where the previous best-performed op-timization strategy fails. We present a family of parameterized quasi-physical simulators that can be both programmed to relax various constraints for task optimization and can be tailored to approximate realistic physics. We tackle the difficult manipulation transfer task via a physics curriculum.

503Limitations. The method is limited by the relatively simple spring-damper503504model for contact constraint relaxation. Introducing delicate analytical contact504505models to parameterized simulators is an interesting research direction.505

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